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# endrich NEWS

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## TURNING POINT



Wolfgang Endrich

The almost two-year Corona crisis taught us that "business as usual" could no longer continue. And since the start of the Ukraine war in February this year, we have painfully felt that Mrs Merkel's policy of "business as usual" has come to an abrupt end. The guiding principle of "change through trade" turned out to be a big mistake. Suddenly we only had crises. Starting with semiconductors, then with gas supply, housing shortage, refugees and so on....

We have unfortunately allowed ourselves to be "lulled" far too much in recent years with the "business as usual" policy. The hope, that it will go on as usual, and we don't need to worry about anything was disastrous for all of us. Our government team was not outstanding, but we were doing relatively well and unfortunately did not realise the global dependencies we had placed ourselves in. Namely, in terms of energy and raw materials from Russia and from China and India, for example, for primary materials for vaccines and medicines. We either didn't see the dangers or didn't want to see them, because Putin had already spoken publicly about his great visions many years ago, but we didn't really take them seriously, because everything was going so well.

The awakening from this sleepiness was terrible and our new government already had its hands full in the first hours of its activity in order to somehow avert or mitigate crises. Perhaps we have not been critical enough all these years to at least consider the crises as a possibility and make appropriate provisions or safeguards.

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Our traffic situation on the roads and the railways, in digitalisation, environmental protection and awareness, the education of our children and finally in the health system are serious failures that could perhaps have been mitigated or even avoided with a look abroad. The Corona crisis, for example, has ruthlessly shown us how old-fashioned our administration still works today.

We have had alarmists for decades who have foreseen climate change, but we have only acted half-heartedly, and it took disasters from flooding, drought and forest fires etc. for us to realise that it was getting serious. For years we have been asleep and have not wanted to see the consequences. Just think of the oceans covered by plastic waste, the poles melting, the glaciers in Europe too.

We have failed to massively promote wind energy and solar energy. Power lines from the North and Baltic Seas to Bavaria have been rejected by the people. The authorities have also contributed to this by approving applications only slowly and sometimes only after years.

Even the health insurance companies have forced the pharmaceutical manufacturers to have the medicines produced abroad through a wrong pricing policy. These are only a few examples of our failures and now we have suddenly been jolted out of our lethargy unprepared. All this certainly hurts tremendously, but it is good to be woken up at last.

What we need now is a spirit of optimism and the will to change and to spit vigorously into our hands. We have had it too good for the last 10 to 20 years. We have learned from those lessons. That is why we must now thoroughly change all that has been neglected in recent years. "MAKE GERMANY GREAT!"



In this spirit, we wish you all a good start, much success in the new year, but also the optimism that with diligence and perseverance a desirable future can be achieved for us and for our children!

# NEWS

## 3<sup>3</sup> SINGLE PAIR ETHERNET

### Freedom of Choices and Budgets

#### What is Single Pair Ethernet?

ALTW's "3<sup>3</sup> SPE" mechanical interfaces are all designed and made according to IEEE 802.3 bp standard offering three mechanical mating interfaces all IP67 up and above, giving you the freedom to choose the interconnects suitable to your needs and requirements for industrial and ruggedized applications.

1. Single Pair Ethernet (SPE) cables simplify the process of connecting and powering edge devices by extending the range and bandwidth of a single twisted pair.

2. SPE cables allow stable, uninterrupted connectivity from remote field devices to the cloud, even in the roughest situations, thanks to excellent shielding and jacketing choices.

3. With the ability to integrate data and power delivery with Power over Data Line (PoDL), you can benefit from increased uptime, process efficiency, and operational benefits.

MPE vs SPE			
	SPEED	DIRECTION	DATA RATE
FAST ETHERNET	100Mbit/s per twisted pair	unidirectional	100BASE-TX
GBIT ETHERNET	250Mbit/s or 2.5Gbit/s per twisted pair	bi-directional	1 GBase-T or 10 GBASE-T
SINGLE PAIR ETHERNET	100Mbit/s or 1 Gbit/s per twisted pair	bi-directional	100BASE-T1 or 1 GBASE-T1

MPE means Multi Pair Ethernet which utilizes two or four wire pairs.



M12 SPE  
(Screw & Push-Pull)



FLOS+ SPE  
(Push-Pull)



X-Lok SPE  
(Push-Lock)

#### APPLICATIONS

- 3 mechanical interfaces IP67 and above for industrial and ruggedized applications
- 3-dom of choices for your needs and requirements
- 3 budgets, pay for what you need

#### FEATURES

- ALTW's proprietary SPE interface integrated in M12 (screw threaded & push-pull) / FLOS+ (push-pull) / X-Lok (push-lock)
- Providing low power & simply networking on end-point sensors
- Cost-effective, smaller & lighter than standard 4 pairs ethernet cable
- Compatible 10/100/1000 Base-T1 data rates as existing technologies \*\*
- Receptacle IPX8 UNMATED waterproof, also available in double ended and field installable
- Vibration resistance 20g (10 ~ 2,000 Hz)
- Supports PoDL (power over data lines)

\*\* 24~26 AWG standard length 15m

## DESIGN OF SYSTEM COOLING USING DC AXIAL FANS

Cooling has a key role in today's electronics, as the lifetime expectancy of passive and active components is highly dependent on the way of transferring the heat generated by their electric current towards the surrounding environment. In some cases, the properly designed PCB and an additional heatsink provides adequate surface to remove the heat emitted by the components, in other cases the system needs active cooling e.g. by forced flow of air. The design of cooling is often not a part of the functional design of the electronic devices, however this has key role in supporting functionality. Usually, a fan used without proper selection may result in oversized mechanical measures, or - in worst case - undersized cooling efficiency. Today's miniaturization trends make it not possible to unnecessarily enlarge enclosure size, while the competition does not allow to produce unreliable products. Therefore, cooling design cannot be started early enough, just like without proper circuit protection, no electronics device can provide its primer functionality for long time without sufficient cooling. Our article is about some important selection criteria of the proper fan depending on the application conditions.

The most important method when taking heat away from components is convection, when the excess thermal energy is released by a flow of the surrounding medium (air/coolant) to the atmosphere. Convection may be natural, when the flow is generated by temperature difference, or forced, when the stream is created by external force such as the rotation of an impeller. Forced convection -provided by high volume airflow of axial fans- is extremely effective towards the cooling of electrical devices. The most important design aspect is to leave sufficient space for this flow around the most heat-critical components concerned, the fan and its power supply, paying special attention at least of the proper air-intake and exhaust vents. If these criteria are taken in consideration during functional design, an important step is taken into the direction of reaching the maximum performance of the application and to avoid later stage compromises between functionality

and sufficient cooling: Although when designing a forced air-cooling system, the proper fan selection depends on many factors, the very first step is always to determine the required air flow volume. This is primarily defined by the total heat generation of the system, and the allowed maximum temperature rise.

In order to calculate the required airflow  $Q$  [ $\text{m}^3/\text{min}$ ], we need to obtain the following values:

- The power dissipated within the systems (worst-case estimation) :  $P_{\text{LOSS}}$  [W]
- The  $k$  constant describing the packing density of the components that prevent the free flow of air ( $k=80-95$  rare placement,  $k=60$  dense components)
- The maximum allowed temperature rise that is defined by the operating temperature range of the used components ( $\Delta T$ )

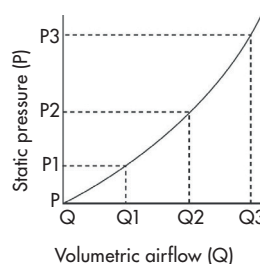
$$Q = \frac{P_{\text{LOSS}}}{C_p \cdot \rho \cdot \Delta T} \cdot k$$

Where,  $Q$ : required airflow [ $\text{m}^3/\text{min}$ ]  $C_p$ : heat capacity of the air at constant air pressure:  $1007\text{J}/(\text{kgK})$   
 $\rho$ : Air density:  $1.2\text{kg}/\text{m}^3 @ 25^\circ\text{C}$

Taking the usual experimental values of the constants in consideration the formula of the required airflow may be simplified like this:

$$Q = \frac{P_{\text{LOSS}}}{\Delta T} \cdot 0.05 \text{ [m}^3/\text{min]}$$

### System impedance curve of an electrical device

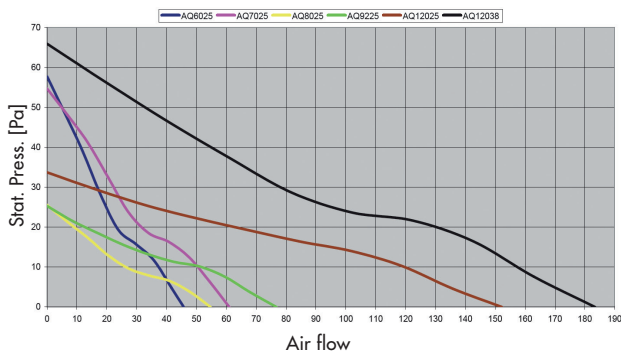


In practice this means that a system dissipating 200W requires  $0.5\text{m}^3$  airflow a minute to keep at maximum  $20^\circ\text{C}$  of temperature rise.

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Although this theoretical calculation provides exact volumetric airflow requirement, it does not give adequate answer for the practical problem, whether the selected fan will provide this airflow or not, since it does not hold enough information about the interaction between the fan and the system to be cooled. It is much more complicated to calculate how a certain cooling fan acts in a specific system arrangement. The characteristics describing the real cooled system's obstruction against the airflow is called the system impedance curve (SIC -fig.1). The system impedance curve describes the static pressure rise over the airflow and can be described by a nearly quadratic equation:  $P_s \sim Q^{1.75...2}$ . It can be generated experimentally by applying various air flow rates to the system and measuring the enclosure pressure it generates.

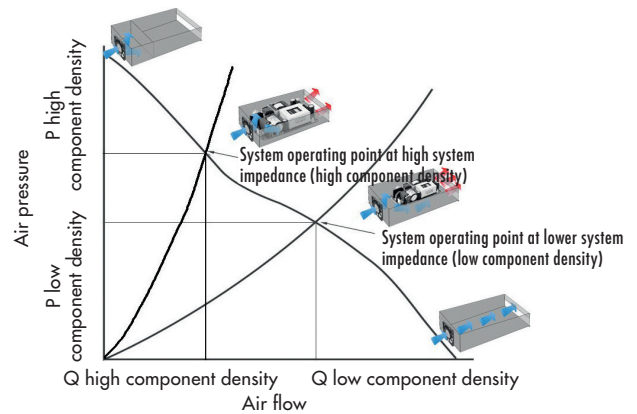


To step forward we need to know the non-linear relationship between the fan's volumetric air flow and its static pressure represented by the characteristic on the 2<sup>nd</sup> figure. The static pressure is maximized when the airflow path is completely obstructed, at this point the volumetric airflow is zero (intersection with Y axis). The maximum possible airflow can be read out at the intersection of the characteristics with axis X, which point represents the case no obstructions at all, free flow of air is enabled (see fig. 3).

In forced convection cooled systems, the above two characteristics play important role. The point of intersection of the fan's air performance (P-Q) curve and the system impedance curve will define the operating point of the cooling solution (fig. 4).

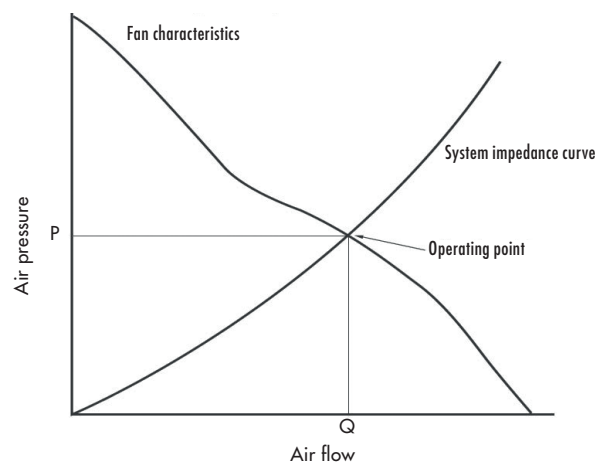
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## Fan's P-Q characteristics and the operating points depending on component density



In case of blocked enclosure, the static pressure grows to the maximum value and the airflow is completely blocked. When there are no obstacles in the air flow path, the theoretical value of static pressure is zero, the volumetric air flow is at maximum. The usual operating point represents a dense packed system and a normal system. In the first case the high system impedance could be only compensated by applying higher pressure, resulting in lower air flow volume. In the other case as the static pressure is lower, higher volumetric airflow is possible, therefore more effective cooling could be done. In both cases we used the same fan, the operating points have been defined by the different system resistances.

## Operating point: intersection of fan's P-Q curve with the system impedance curve of the enclosure



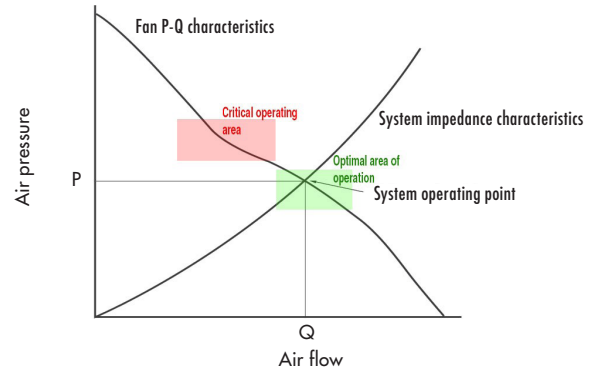
By knowing above fact it is now possible to select the proper fan. Nowadays DC fans are more popular than AC versions as their power consumption is usually lower, lifetime is longer, and because their angular speed is proportional to their supply voltage, it is easy to apply speed control. The lower the speed the more silent the operation is, the lower the power consumption and the higher the lifetime will be (due to reduced wear out of the bearing). DC fans produce less EMI than AC versions, there are no geographical issues of supply voltages and frequencies, and price differences already disappeared. Therefore, we only write about DC axial fans in this paper. After calculating the required air flow rate, having the system impedance curve on hand, we define the static pressure interval, that should be overcome by the fan to provide the required air volume. Then using the fan manufacturers' catalogues, a specific device can be selected, that is able to provide the adequate airflow on the level of back pressure required by the SIC. It is advised to select the operating point out of the critical area marked by red on figure 5. This area is the so-called stall area, where the air flow stalls at the blade profile, which makes negative effects. Such an immediate disadvantage is the considerable increase in noise. For longer term negative effect is the vibration, which can reduce functionality and leads to lifetime issues. Therefore, fan should always be operated in the optimum operating area marked with green on figure.

Further reducing noise at even the optimum operating area can be also important selection criteria, it is advised to select the fan with the highest possible diameter. Bigger sizes mean lower speed, therefore less bearing noise. This is however against today's miniaturization trends, we should use small, thin fans wherever and whenever possible. It is important to consider size at the beginning, this is not only the question of design and technology trend but on long term influences price of the end-product.

If the desired operating area cannot be reached by a single small fan, it is possible to use multiple fans next to or behind each other. These arrangements will negatively influence noise and mathematical lifetime expectancy, but offer redundancy, which supports system reliability.

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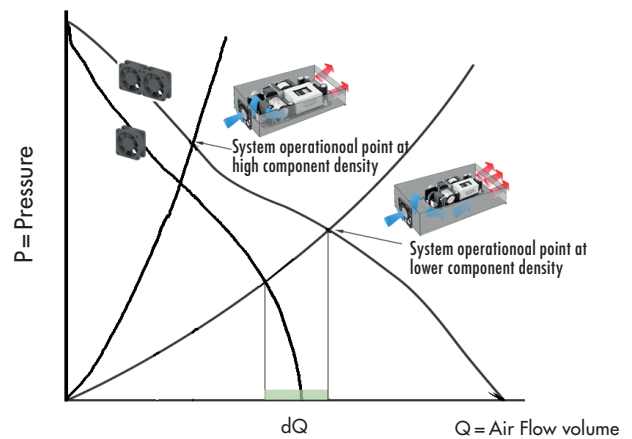
## Area of operating points



## Using multiple fans – parallel operation

When we switch several fans in parallel (side by side), then the joint system's air moving capacity is increased in the range of low static pressures. On the curve on fig.6, it can be observed that when used concomitantly, the idle air flow is increased. In practice, this means that we can operate with such an arrangement if the component density of the system to be cooled is low, so the operation point can be set at a low static pressure level. Of course, the new working point is also associated with a slightly higher air pressure, however, where a significant increase is observed it is the air flow. In the case of higher system impedance, this arrangement does not bring much benefit since the additional investment does not result in a significant increase in airflow.

## Characteristics of parallel fan organization



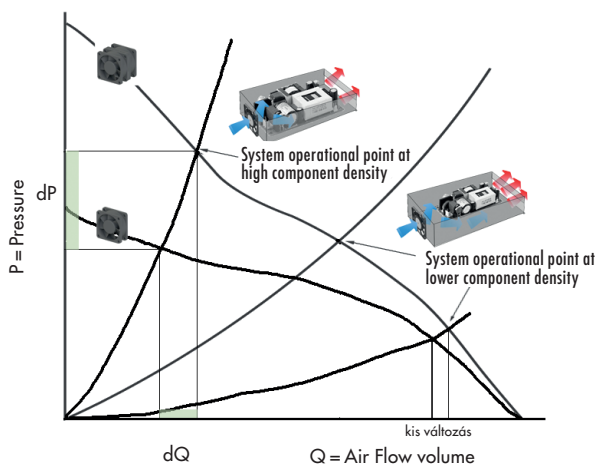
## Using multiple fans – serial operation

When several fans are connected in series (behind each other), the airflow of the combined system increases

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significantly in the range of high static pressures, so with such an arrangement we can achieve a significant improvement in chassis with high component density and high system impedance. In this case, the operational point is in an area characterized by high static pressure, the serial arrangement is characterized by increased air flow even at higher air pressure. At low component densities, this additional pressure is not needed, so this arrangement cannot be applied economically, because the investment will not bring a significant increase in air flow (see fig. 7).

## Characteristics of serial system



## The effect of speed on air flow

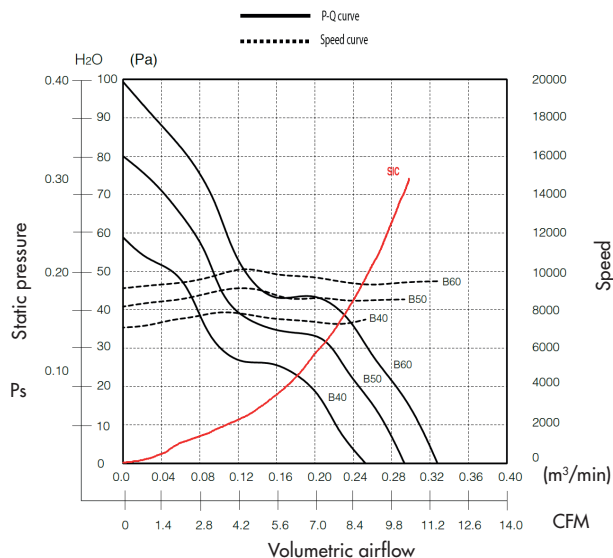
DC axial fans have different P-Q characteristics for different nominal supply voltages, so they differ at nominal rotational speeds (see Fig. 8), so when applied to the same system at a higher rotational speed, they can be used to achieve greater air flow and pressure. Assuming the impedance curve being a square function, the working points that are output for each rotational speed can be assigned to higher static pressure and air flow values, respectively. Variable speed can be achieved with external voltage regulation for two-wire fans, but of course there are built in RPM control functions at three- or four-wire fans. In the case of the former, the third wire is used to receive a high-frequency pulse width modulation control signal (PWM), while in the case of the latter, a so-called additional tachopulse supplied by a (HALL) transmitter is received from the motor on the fourth wire. The fan returns data about its speed to the external control

electronics. On this line, in addition to the usual data, a special distress signal, such as a warning of possible rotor jamming, may also be received. Pulse width modulation speed control is actually a supply voltage control, the essence of which is that the DC voltage applied to the fan terminals is periodically alternated between the values of 0V and the rated voltage, using transistor or FET-based electronics. The effective value of the terminal voltage is determined by the ratio of times spent in the two states (fill factor).

From the foregoing, some very important conclusions can be made, which must necessarily be taken into account when choosing a cooling fan.

With an increase in speed

- (+) the airflow increases
- (+) squared increase in pressure occurs
- (-) there is a significant increase in noise,
- (-) significantly increased engine heating
- (+) the bearing load reduces the service life



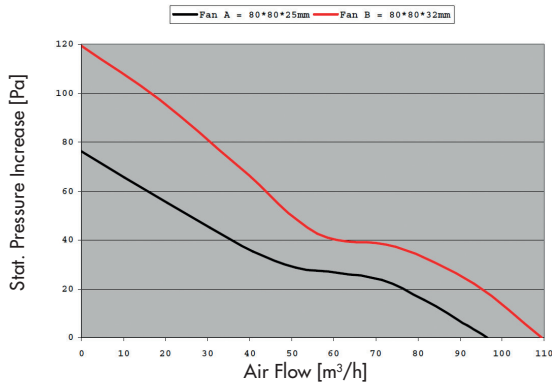
We would like to show their significance through an example. Figure 9 shows the P-Q characteristics of two cooling fans. The parameters of the fans are as follows:

- A: 80x80x25 mm; 4200 rpm; 3.96 W; 44 dB(A)
- B: 80x80x32 mm; 4600 rpm; 4.20 W; 46 dB(A)

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## 80 mm Fan Size



In the example above, in terms of the physical dimensions of the two devices, there is only a difference in their thickness. It is assumed that the device marked B would provide sufficient cooling for the system, but for space-saving reasons, we choose the thinner design (A). To ensure proper volumetric airflow and pressure levels, fan A is used at ~10% higher RPM, which results in 31.4% higher consumption, greater dissipation (heating), significant additional noise and significantly reduced service life due to the increased load on the bearing. The negative impact of warming further worsens life expectancy, which is really evident, when you consider the fact, that - according to some experts - the fan motor's 10°C durable temperature increase causes 20,000 hours (approx. 40%) reduction in lifespan.

From the above, it can be seen, when choosing cooling solutions for a particular system, it is worth making a reserve of the required airflow, using a cooling fan with the largest possible physical size, running at a speed even lower than the nominal one, if the design of the system allows it. If for some reason a higher static pressure or a larger volumetric air flow is required, depending on the layout, there are several options: you can raise the number of revolutions and/or apply more than one cooling fans (in serial or parallel arrangement). In all these cases, it is necessary to carefully examine the actual additional advantages of the given solution and how much investment it requires, because it often happens with poor designs that, for example, the self-heating of the applied several fans is greater than the extra cooling it offers for the system. In addition, the economy must also be examined, the price of the second, third fan, the increase in the mathematical probability of failure, the increase in consumption all affects the price and operating costs of the final product.



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